Linee di trasmissione

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A.A. 2020-21



Map of the 1858 trans-Atlantic cable route



Great Eastern at Heart's Content







Il cronometro di John Harrison





Un cavo coassiale RG58/CU, con conduttori in rame stagnato, isolato con polietilene (PET) e con guaina esterna in polivinilcloruro (PVC) nero.







Cavo coassiale RG59 doppio



Cavo coassiale RG59 miniatura



Cavo coassiale RG59B/U



Cavo coassiale RG59B/U LSF



Cavo coassiale RG62 miniatura



			$p = \frac{a}{d}$ $q = \frac{a}{D}$	Formulas for a < b							
Capacitance C, farads/meter	$\frac{2\pi\epsilon}{\ln\left(\frac{r_0}{r_i}\right)}$	$\frac{re}{\cosh^{-1}\left(\frac{s}{d}\right)}$		e b a							
External inductance L, henrys/meter	$\frac{\mu}{2\pi}\ln\left(\frac{r_0}{r_i}\right)$	$\frac{\mu}{\pi}\cosh^{-1}\left(\frac{s}{d}\right)$		# <mark>a</mark>							
Conductance G, siemens/meter	$\frac{2\pi\sigma}{\ln\left(\frac{r_0}{r_i}\right)} = \frac{2\pi\omega\epsilon''}{\ln\left(\frac{r_0}{r_i}\right)}$	$\frac{\pi\sigma}{\cosh^{-1}\left(\frac{\vartheta}{d}\right)} = \frac{\pi\omega\epsilon''}{\cosh^{-1}\left(\frac{\vartheta}{d}\right)}$		$\frac{a}{a} = \frac{\omega e''b}{a}$							
Resistance R, ohms/meter	$\frac{R_s}{2\pi} \left(\frac{1}{r_0} + \frac{1}{r_i} \right)$	$\frac{2R_s}{\pi d} \left[\frac{s/d}{\sqrt{(s/d)^2 - 1}} \right]$	$\frac{2R_{a1}}{rd} \left[1 + \frac{1+2p^2}{4p^4} (1-4q^2) \right] \\ + \frac{8R_{a1}}{rD} q^2 \left[1 + q^2 - \frac{1+4p^2}{8p^4} \right]$	2 <i>R</i> .							
Internal inductance L _i , henrys/meter (for high frequency)	$\stackrel{R}{\smile}$										
Characteristic impedance at high frequency Z ₀ , chms	$\frac{\eta}{2\pi}\ln\left(\frac{r_0}{r_i}\right)$	$\frac{\eta}{\pi} \cosh^{-1}\left(\frac{s}{d}\right)$	$\frac{\frac{\eta}{\pi} \left\{ \ln \left[2p \left(\frac{1-q^2}{1+q^2} \right) \right] - \frac{1+4p^2}{16p^4} \left(1-4q^2 \right) \right\}$	7 <u>6</u>							
Z ₀ for air dielectric	$60\ln\left(\frac{r_0}{r_i}\right)$	$120 \cosh^{-1}\left(\frac{s}{d}\right) \simeq 120 \ln\left(\frac{2s}{d}\right)$ if $s/d \gg 1$	$\frac{120\left\{\ln\left[2p\frac{(1-q^3)}{(1+q^3)}\right]\right.}{-\frac{1+4p^3}{16p^4}(1-4q^3)\right\}}$	$120\pi \frac{6}{b}$							
Attenuation due to conductor α_c	4	\leftarrow $\frac{R}{2Z_0}$ \rightarrow									
Attenuation due to dielec- tric as	4	$\longleftarrow \qquad \qquad$									
Total attenuation dB/meter	4	<									
Phase constant for low-loss lines β	4	$\longleftrightarrow \qquad \qquad$									

All units above are mks. $\epsilon = \epsilon' - j\epsilon'' = \text{permittivity, farads/meter}$ $\mu \neq \text{permeability, henrys/meter}$ $\overline{\gamma} = \sqrt{\mu / \epsilon} \text{ ohms}$

 $e'' = \log factor of dielectric = \sigma \cdot / \omega$

 R_{*} = skin effect surface resistivity of conductor, ohms

 $\lambda =$ wavelength in dielectric

Formulas for shielded pair obtained from Green, Leibe, and Curtis, Bell System Tech. Journ., 15, pp. 248-284 (April 1936).

for the dielectric



1. The UHF connector can still be purchased from some manufacturers today.



3. The BNC connector is often found in test instruments.



1. The SMA connector is one of the most common connector types used for RF/microwave applications.

1mm	110 GHz						20	
1.85mm	67 GHz							Ö 🎽
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1.0/2.3 • SMC	10 GHz						Ð	
GR874	9 GHz							
MCX-75 • UMCX • 7/16 • OSMT	6 GHz							
MMCX • OSX • PCX • MCX	6 GHz							
HN • SMB • FAKRA	4 GHz							C
BNC • SMB-75 • MINI SMB-75	4 GHz							
F	3 GHz							
MINI UHF	2.4 GHz							Z
10-32	2 GHz							
N-75	1.5 GHz							
LC • 1.6/5.6	1 GHz							
BNC-75 • TNC-75	1 GHz							
UHF	300 MHz							
TWINAX - FME	200 MHz							
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references&tools



Fig. 4. Equivalent circuit of series gap in strip line (center line representation).

(1)
$$b_1 = \frac{D}{\lambda'_0} \ln\left\{\cosh\left(\frac{\pi S}{2D}\right)\right\}$$